

CAHRS Workshop

Testing for Crash & Safety Simulation

Hubert Lobo
DatapointLabs
New York, USA

DatapointLabs

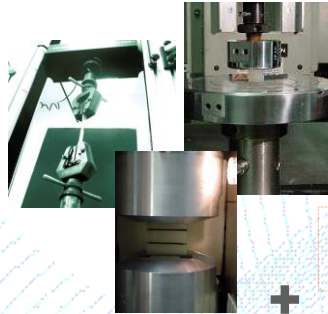


- Research quality material testing
- ISO 17025 production environment
- Results in 5 days (48 hour RUSH service)
- Web-based quotation & data delivery
- Domain expertise in CAE material calibration

expert material testing



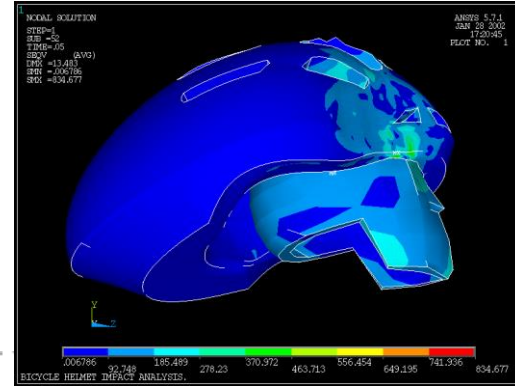
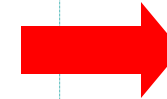
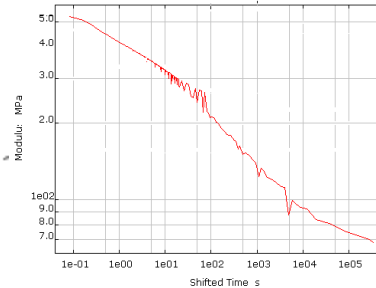
materials



testing

+

data conversion



Your CAE

- **TestPaks[®] = Materials testing + CAE material parameter conversion**
 - ▶ metal, plastic, foam, rubber, composites...
 - ▶ over 20 CAE software codes

TestPaks.com



DatapointLabs

Topics

- A test philosophy for representing rate dependency of materials
- Experimental technique including sampling and specimen geometries
- Assessment of crash material data quality, expected trends & validation
- Specific comments for unfilled and fiber-filled polymers, foams, rubber and metals.

Getting pertinent properties

- Importance of measuring the right property
- Artifact free data
 - ▶ Properly designed experiments
 - ▶ eg. not using crosshead displacement to calculate strain
- Traceable data (ISO 17025)
 - ▶ NIST traceable instruments
 - ▶ Certified trained technicians

Getting the right samples

- **Spatial variation**
 - ▶ Properties vary with location
 - ▶ Forming, stretching, molding...
- **Environmental variation**
 - ▶ Ageing and conditioning
- **Process variation**
 - ▶ Degradation from processing
 - ▶ Recycled materials

Metals

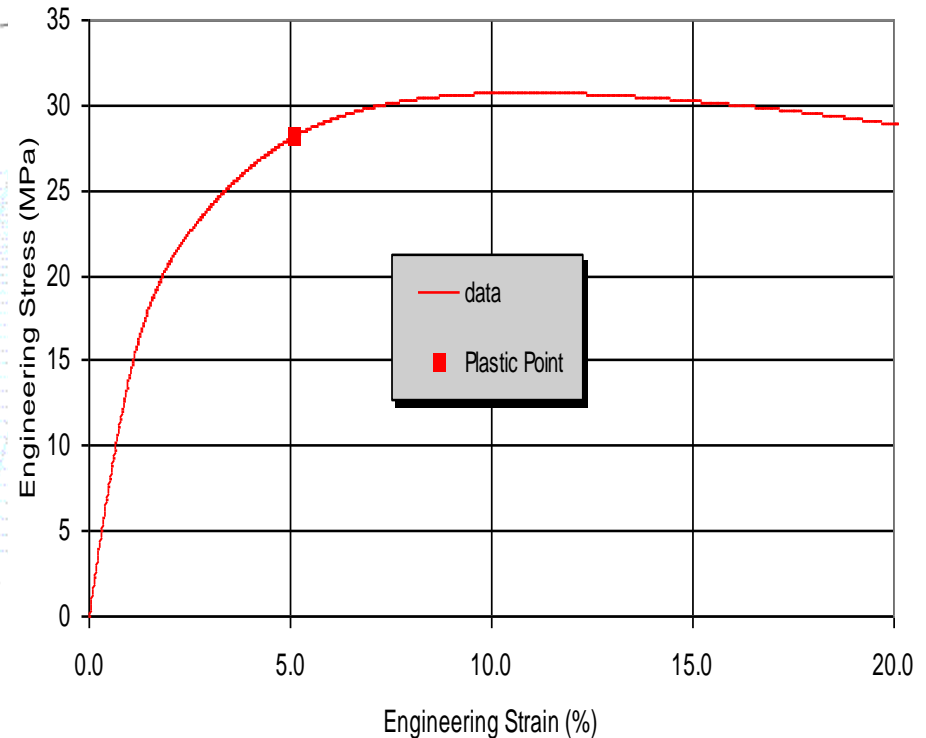
- Relatively well behaved
- Models designed to match behavior
- Challenges lie with post yield non-Mises failure envelopes
- Scaling of yield surface with strain rate
- Work of Nakajima, Dubois, Hooputra

Plastics

- Not well behaved
- Models not designed for plastics crash simulation
- Complex models are expensive
- Can we develop best practices for adapting common models to plastics

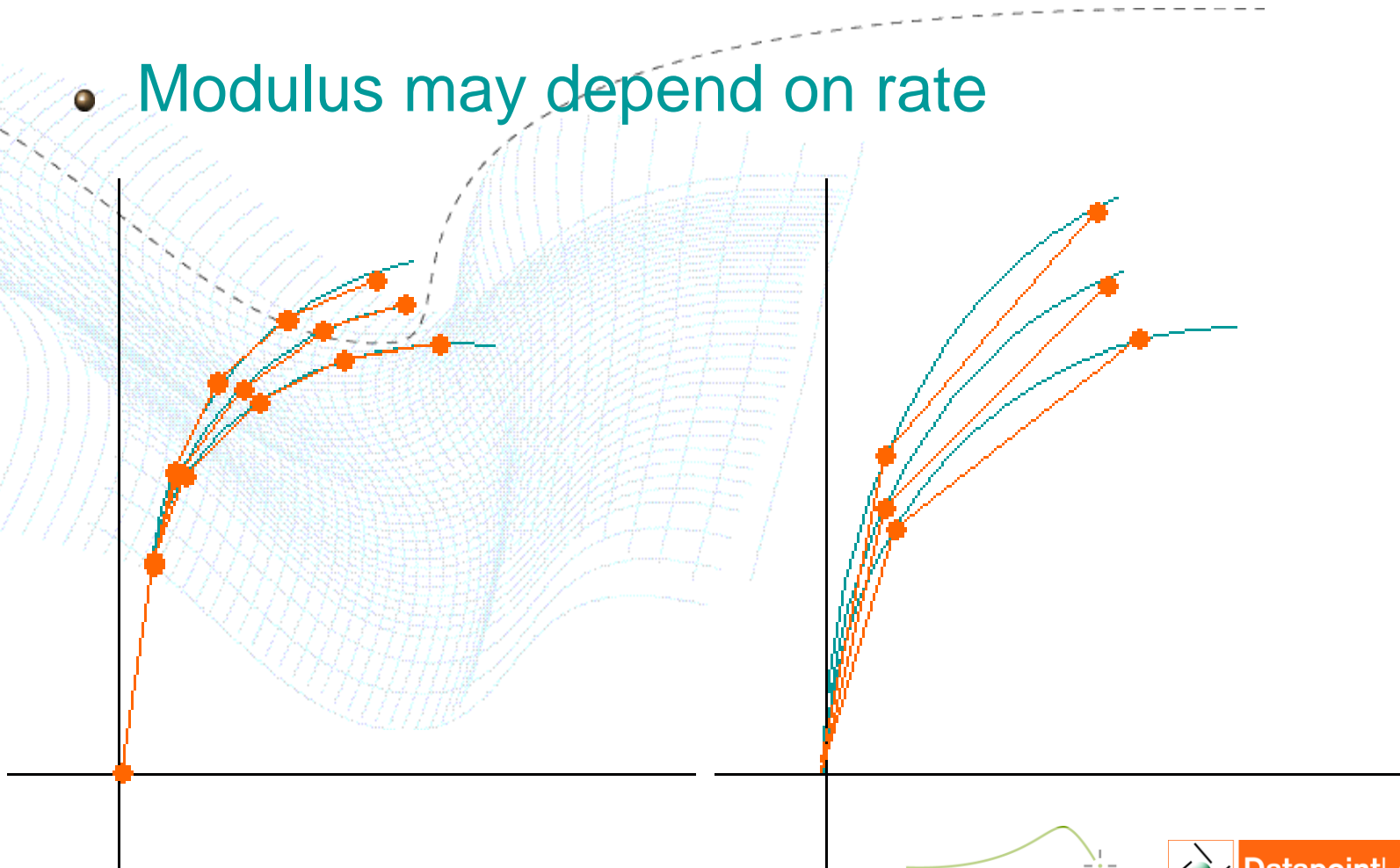
Plastics Behavior - Basics

- Non-linear elasticity
- Elastic limit well below classical yield point
- Significant plastic strains prior to yield
- Post-yield with necking behavior



Plastics Rate Effects

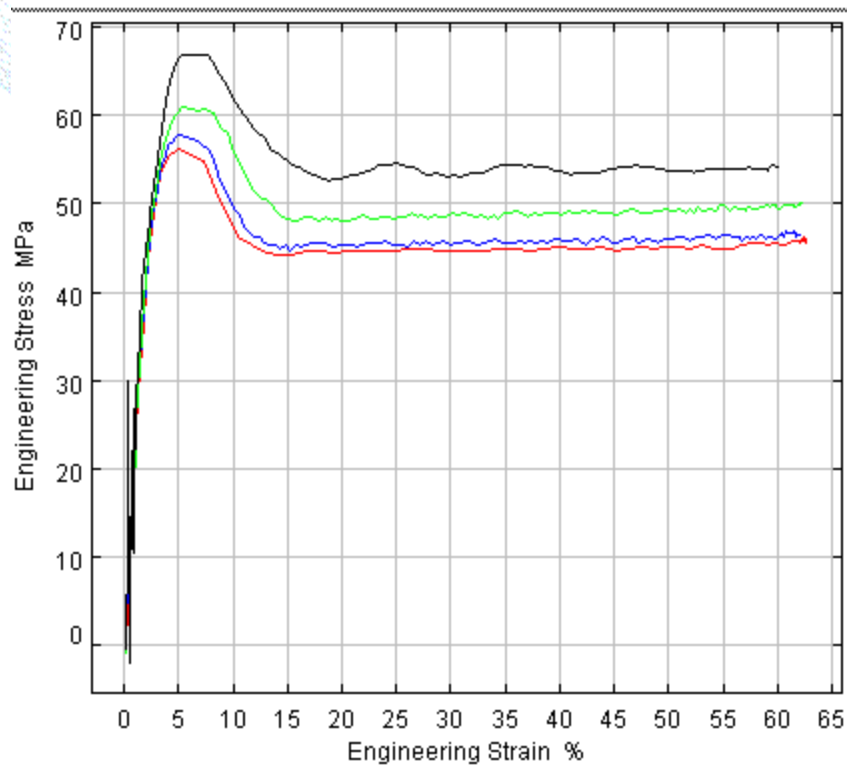
- Modulus may depend on rate



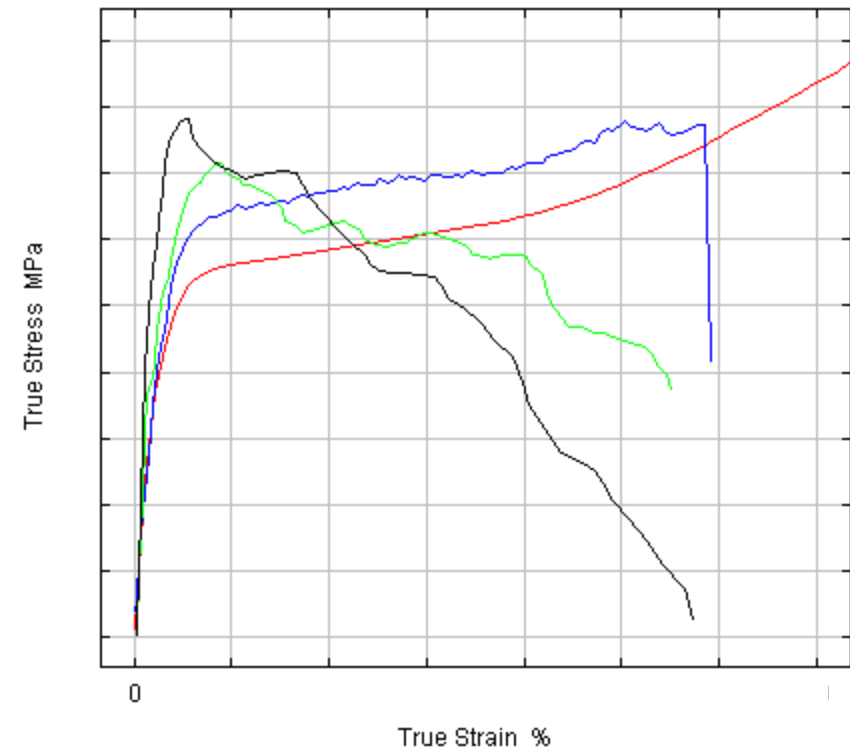
Plastics Rate Effects

● Fail strain may be rate dependent

Engineering Tensile Stress-Strain Curves



True Tensile Stress-Strain Curves



Material Testing

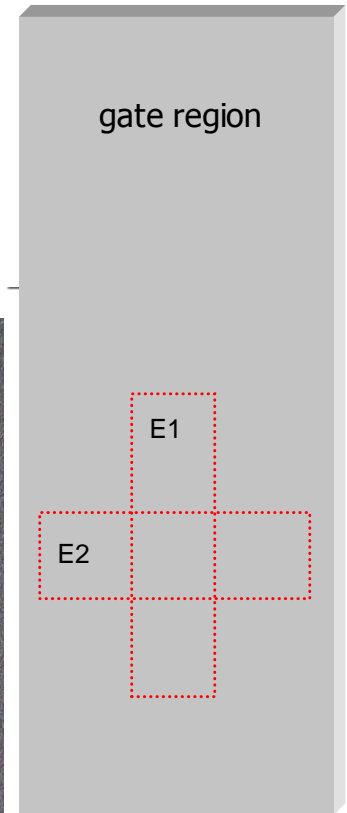
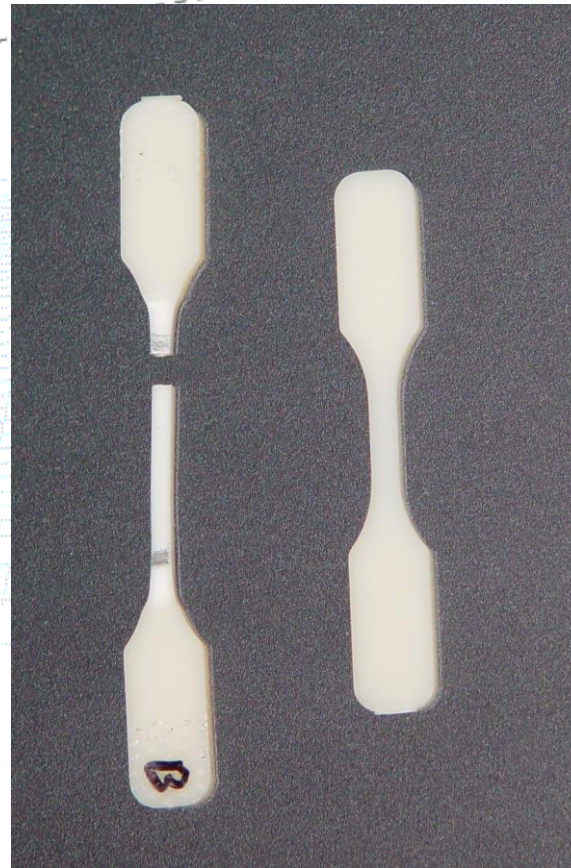
- Instron servo-hydraulic UTM
- Dynamic load cell
- Test at 0.01, 0.1, 1, 10, 100/s strain rates
- Temperatures: -40 to 150C

tens_slow.mpg

Tens.mpg

Test Specimens

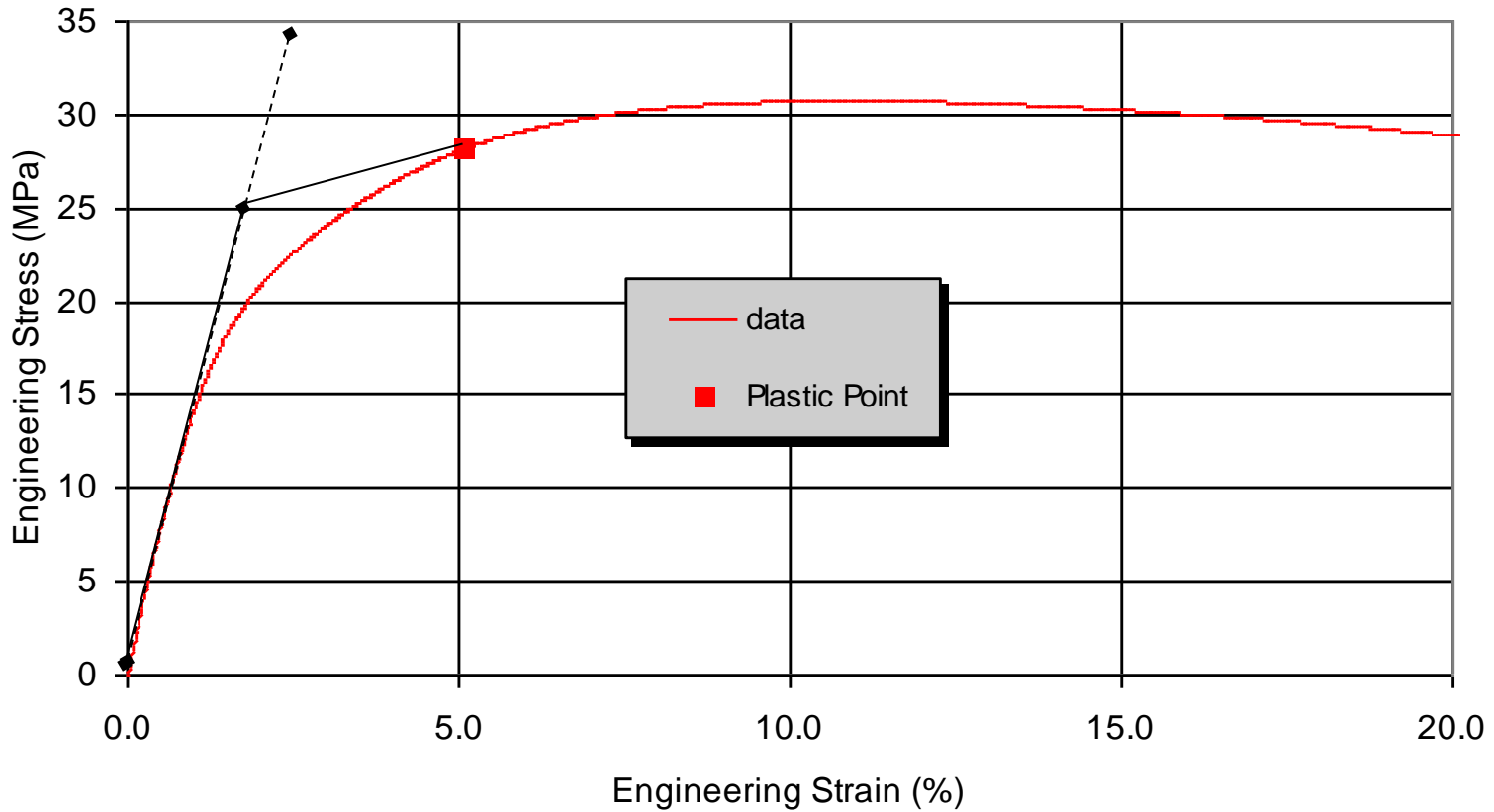
- ASTM D638 Type V
- Preparation
 - ▶ CNC from plaque
 - ▶ CNC from part
 - ▶ Molded
- Variability
 - ▶ processing
 - ▶ orientation
 - ▶ thickness



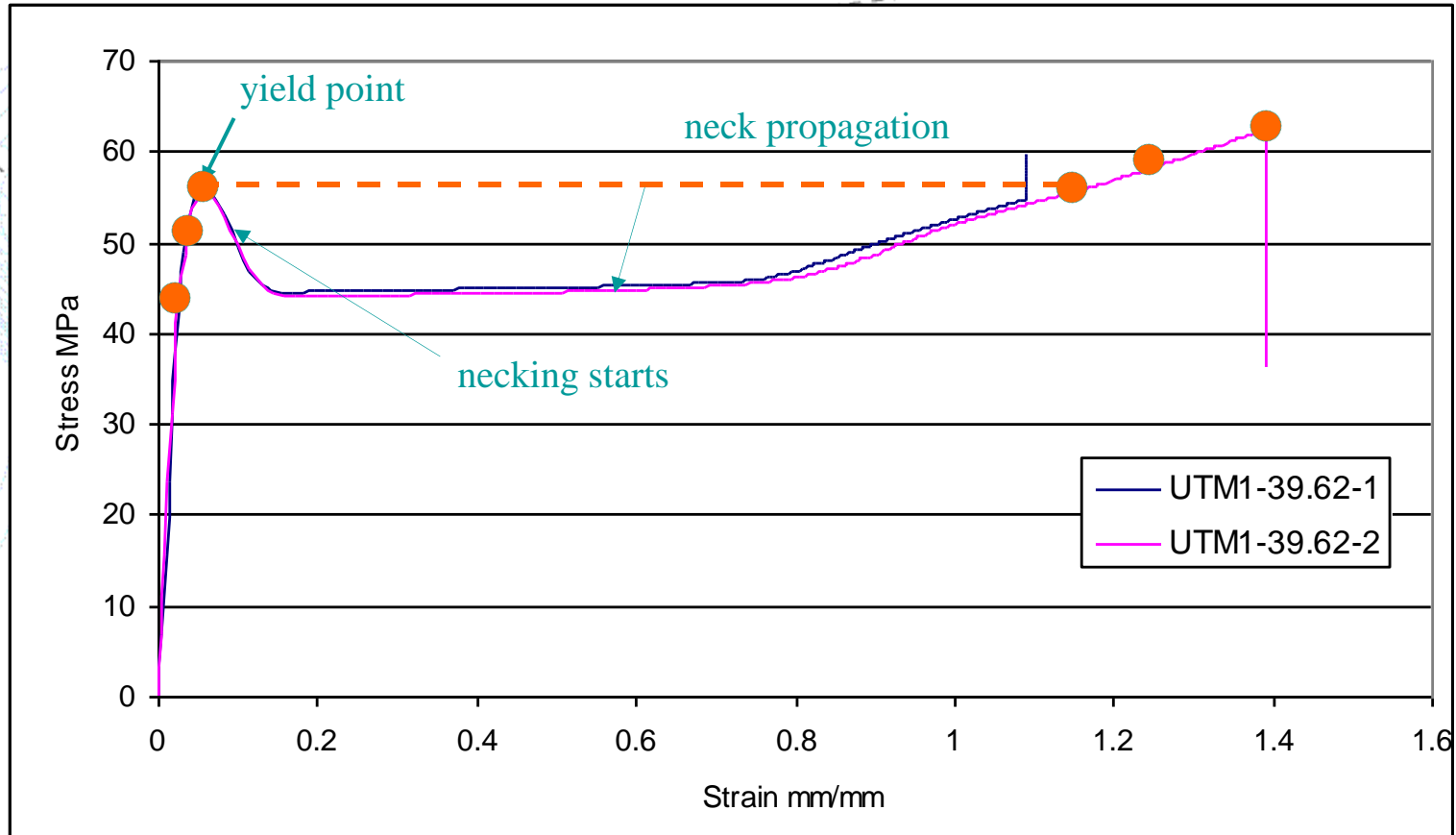
Modeling simple ductile plastics

- Modulus is not rate dependent
 - Large strains to failure
 - Post-yield necking
 - Plasticity curves vary with strain rate
 - Failure strain independent of strain rate
-
- LS-DYNA, ANSYS, ABAQUS, PAMCRASH

Choosing EMOD



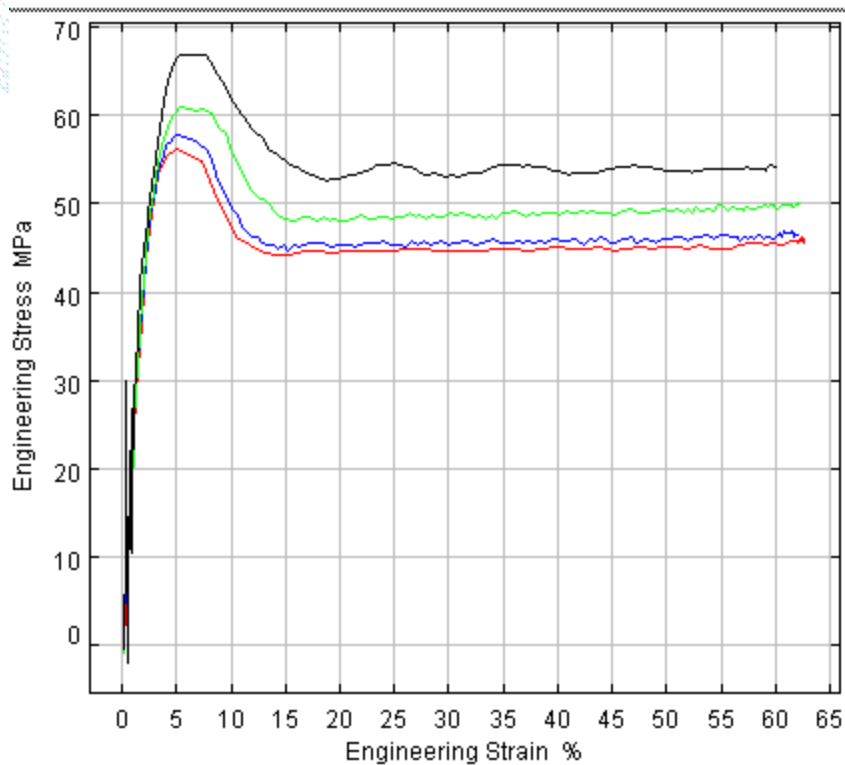
Post-yield with necking (DeiHL)



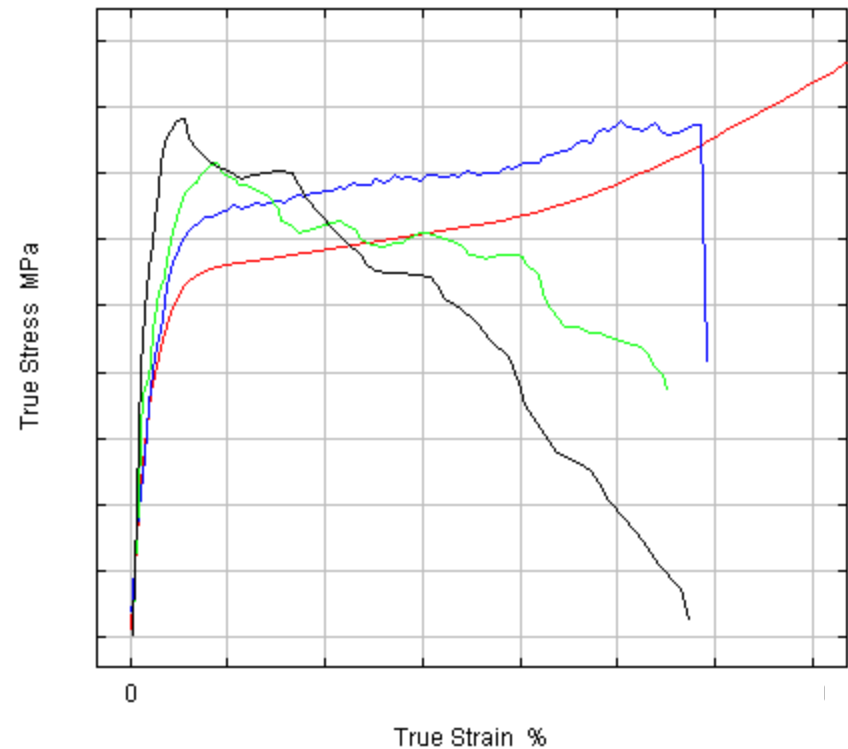
Fail Limitations

When FAIL f(strain rate)

Engineering Tensile Stress-Strain Curves



True Tensile Stress-Strain Curves



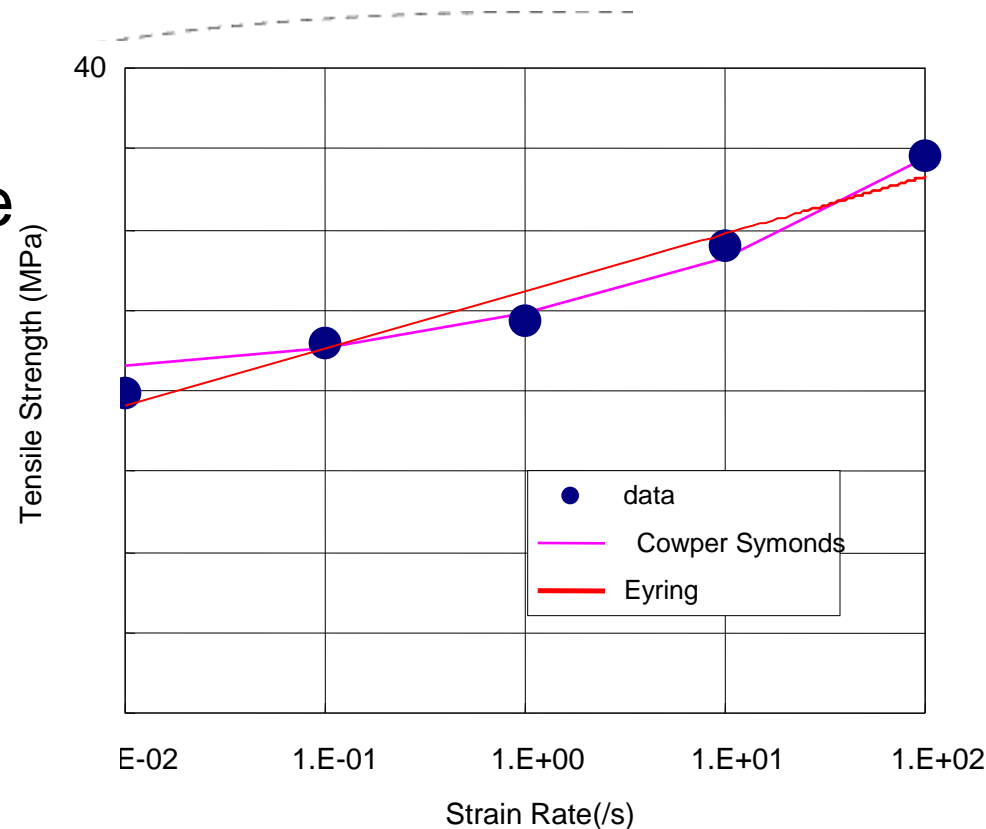
Modeling Rate Dependency

Cowper Symonds

- ▶ Does not correlate well with plastics rate dependency

LCSR

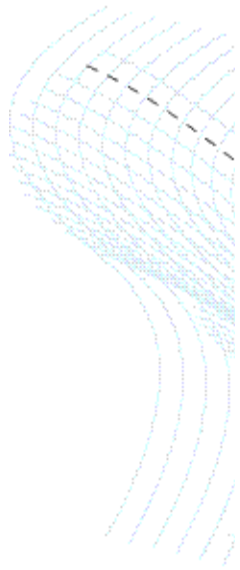
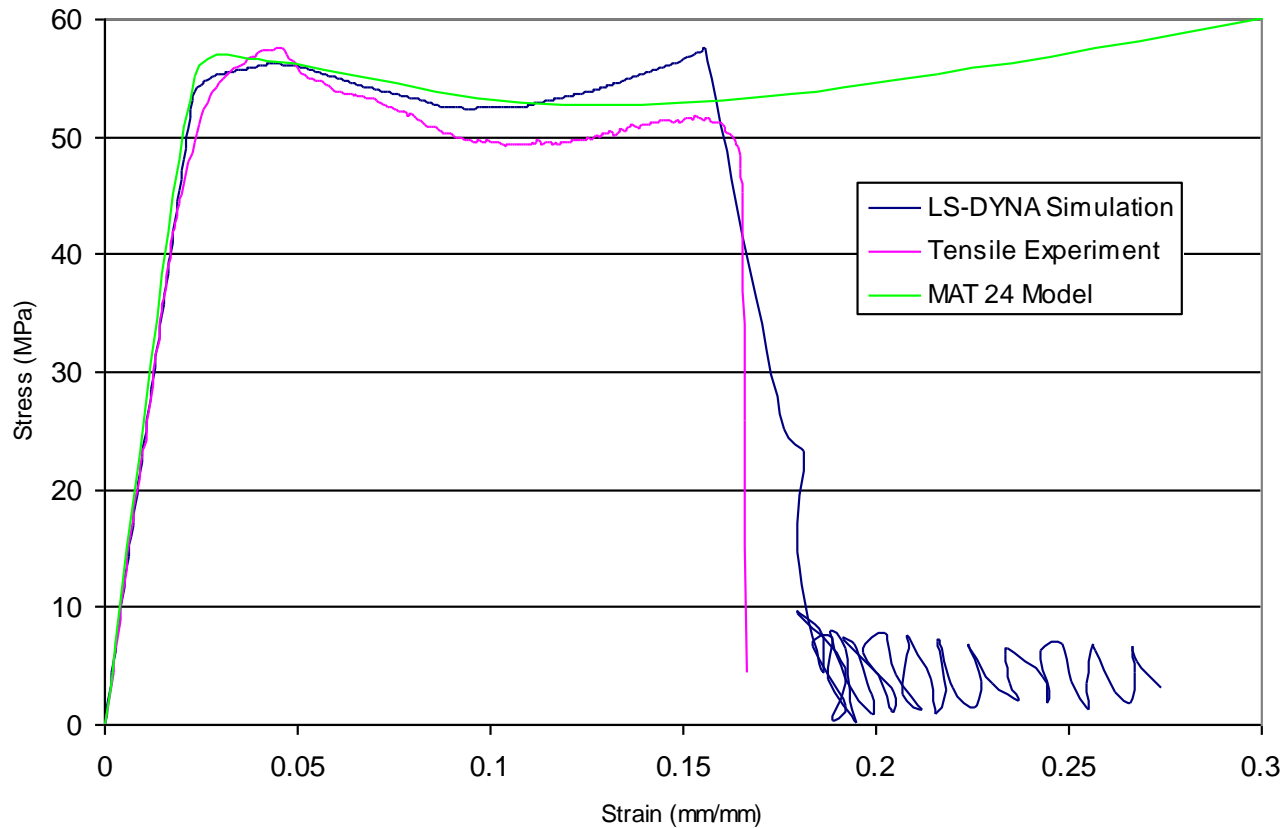
- ▶ Capture model independent behavior



Eyring Model

- Eyring Model
 - ▶ Yield stress v. log strain rate is linear
 - ▶ Best form for plastics
- Fit yield stress v. log strain rate data to Eyring equation
- Can submit to LSDYNA MAT24 as table using LCSR

MAT24 validation

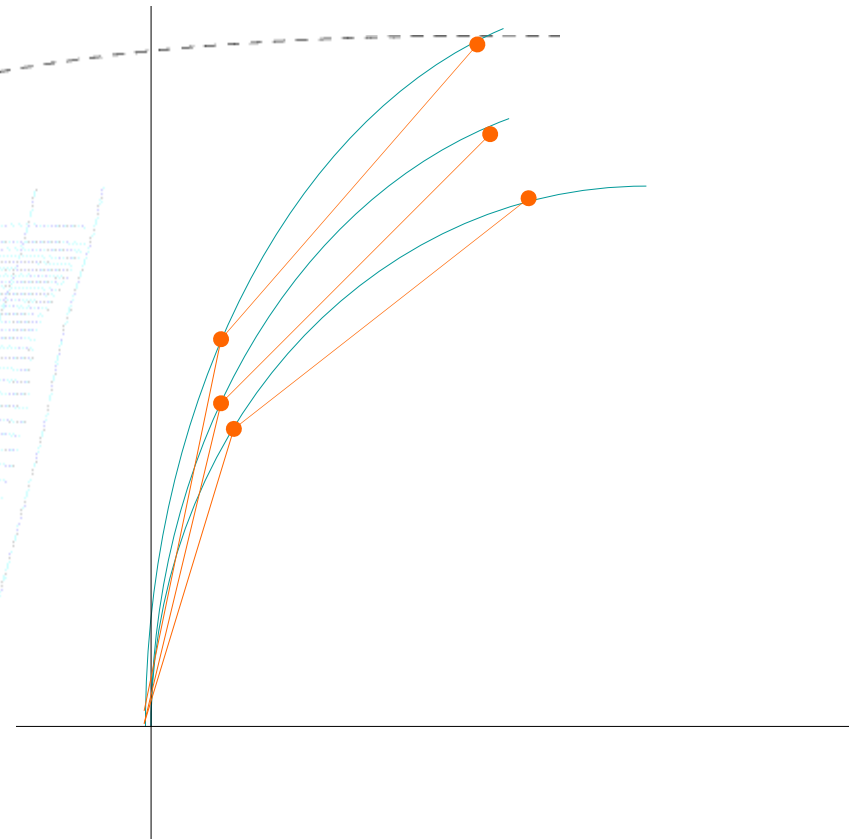


Brittle plastics

- Modulus is rate dependent
- Small strains to failure
- Brittle failure
- Failure strain decreases with increasing strain rate
- LSDYNA MAT19

Methodology for MAT 19

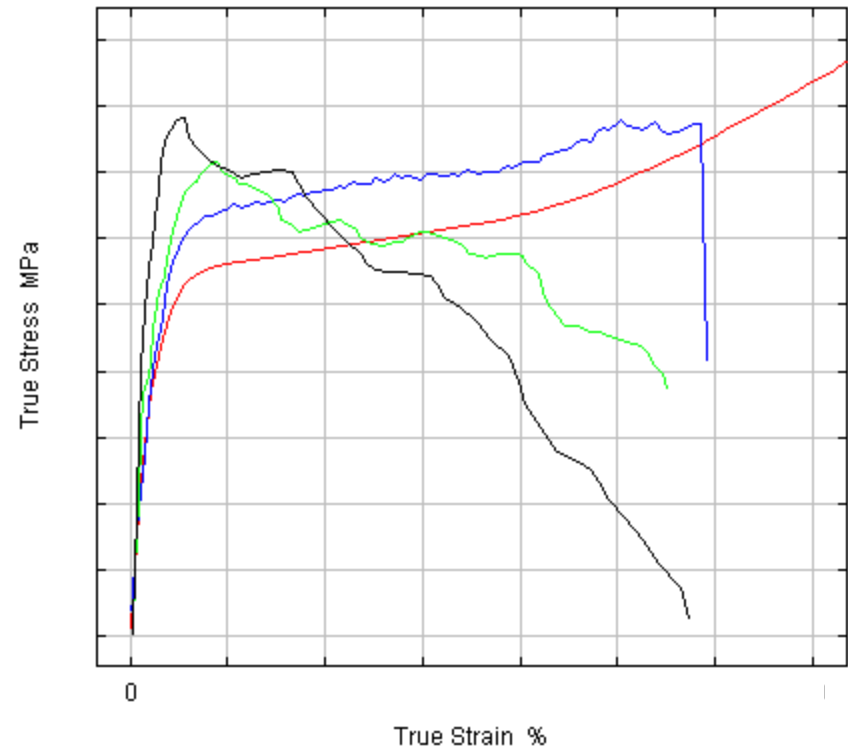
- Determine elastic limit at quasi-static strain rate
- Use elastic limit for von-Mises yield
- Define failure
 - ▶ failure stress v. strain rate table



Ductile-brittle transitions

- Non-linear behavior
- Failure depends on strain rate
- Models
 - ▶ LS-DYNA MAT89
 - ▶ PAMCRASH 103
 - ▶ Abaqus *ELASTIC
*PLASTIC,Rate

True Tensile Stress-Strain Curves

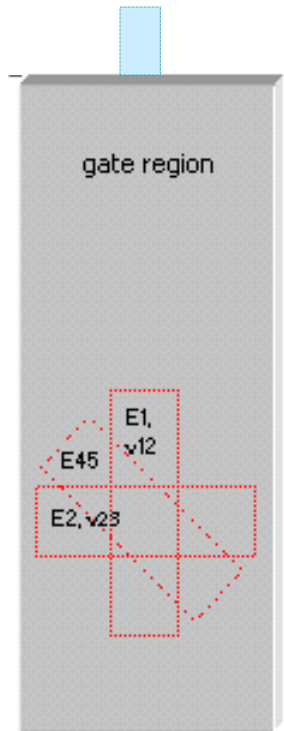


Fiber Filled Plastics

- **Digmat MX**
 - ▶ Material model reverse engineered from standard experiment
- **Perform injection-molding simulation**
- **Apply Digmat material model to transfer data to crash simulation**
- **Crash model has spatially oriented properties**

Basic Digimat *TestPak* Protocol

- Mold 100X300X3.16mm plaques
 - ▶ Edge gated on 100 mm end
 - ▶ Long flow length
 - ▶ Fully developed flow
 - ▶ Highly fiber orientation
- Cut test specimens by CNC
- 5 specimens each (0°, 90°)
- Obtain true stress-strain data



Advanced Models

- MATSAMP (LS-DYNA)
- Standard rate dependent model
- Add non-mises failure envelope
 - ▶ Compression
 - ▶ Shear
- Add triaxiality
 - ▶ Post yield transverse strain
- Add unloading

Pros and Cons

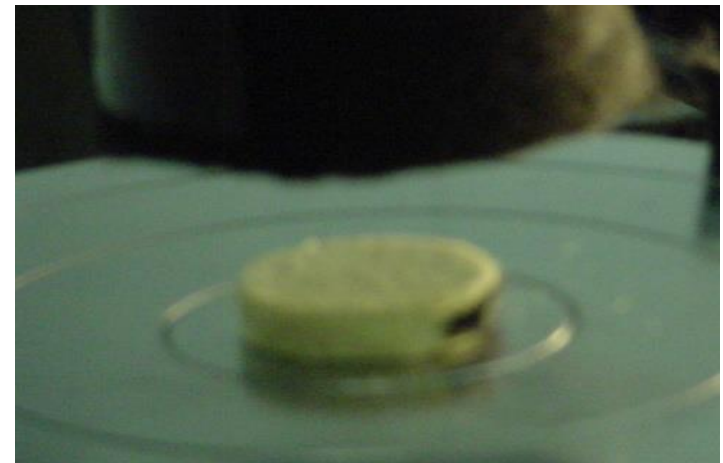
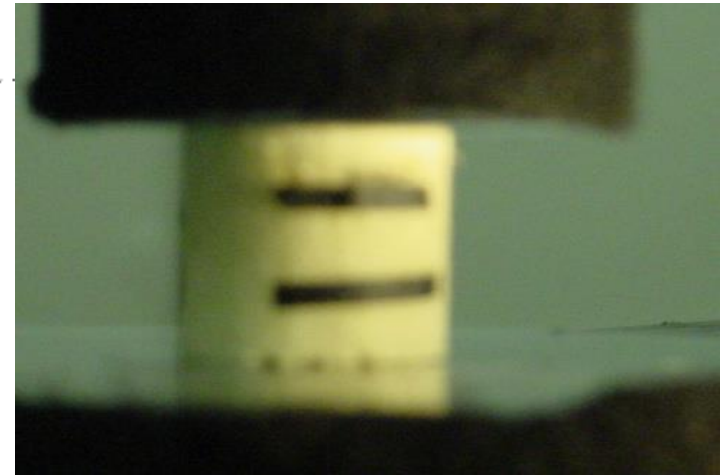
- Better failure envelope modeling
- Greater cost
- More complex model
- Greater simulation accuracy in difficult cases
- Cost-benefit not certain for general use

Foams

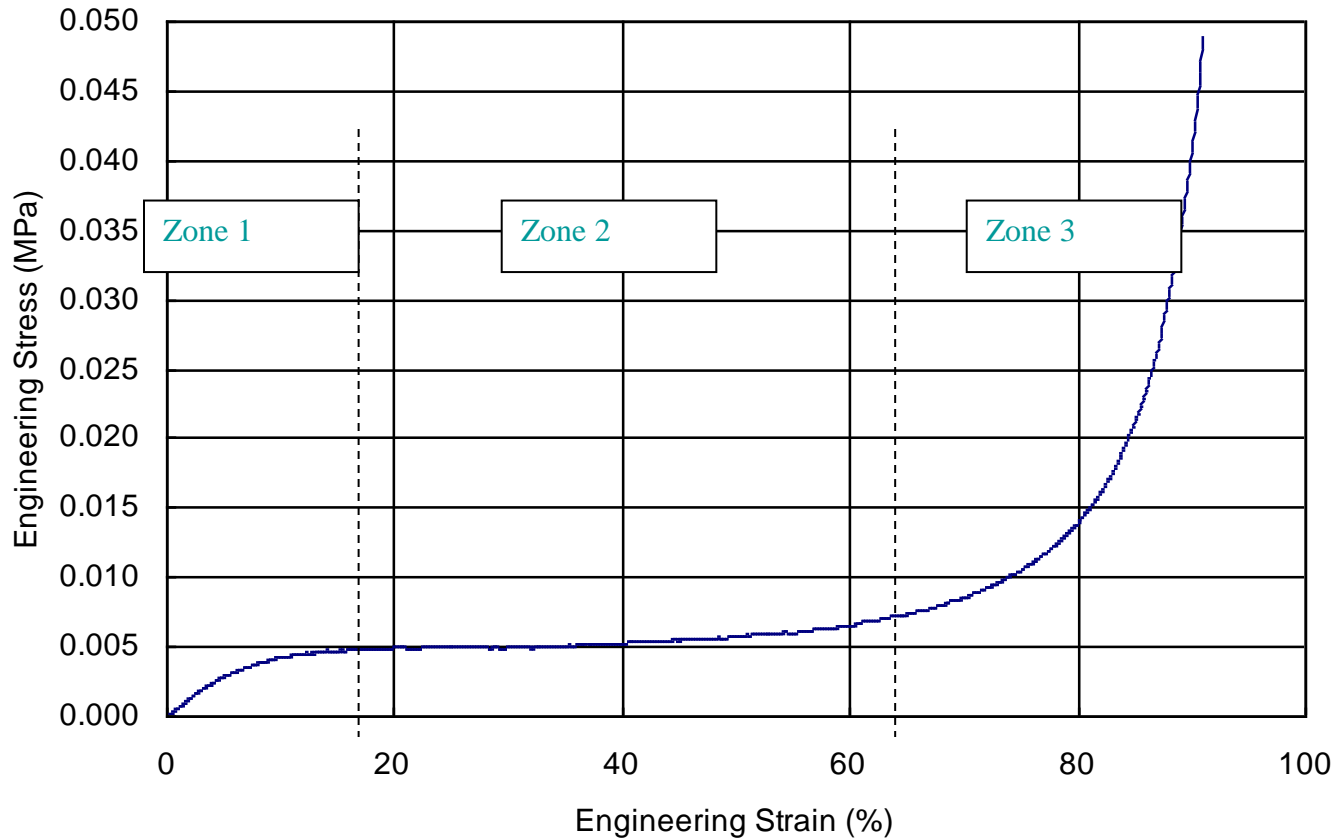
- Different deformation modes
 - ▶ Crushable
 - ▶ Elastic with or without damage
 - ▶ Visco-elastic
- Large volumetric strain component

Effect of Poisson's Ratio = 0

- Material compacts by eliminating air
- No lateral deformation
- Poisson's Ratio $\rightarrow 0$
- Axial strain \cong volumetric strain
- True for
 - ▶ open cell foams
 - ▶ crushable foams
- May not be true for
 - ▶ closed cell foams
 - ▶ elastomeric foams

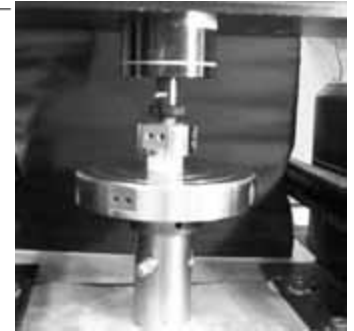


Typical Stress-Strain Data



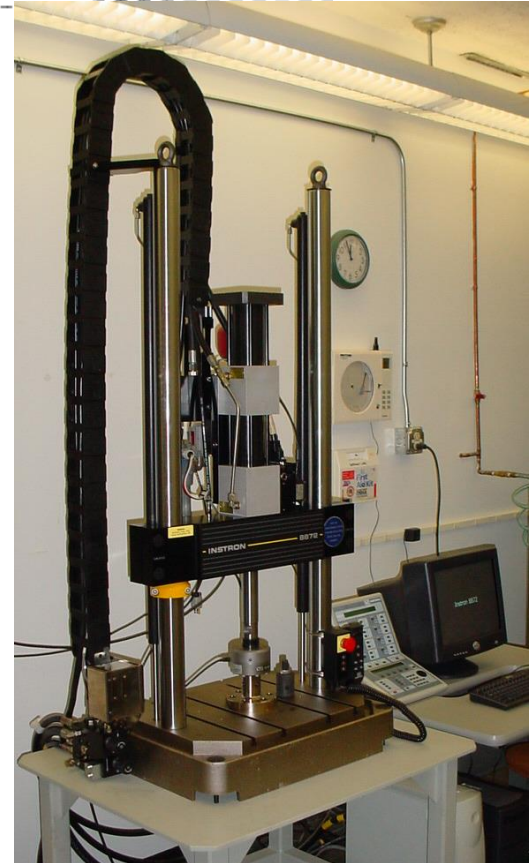
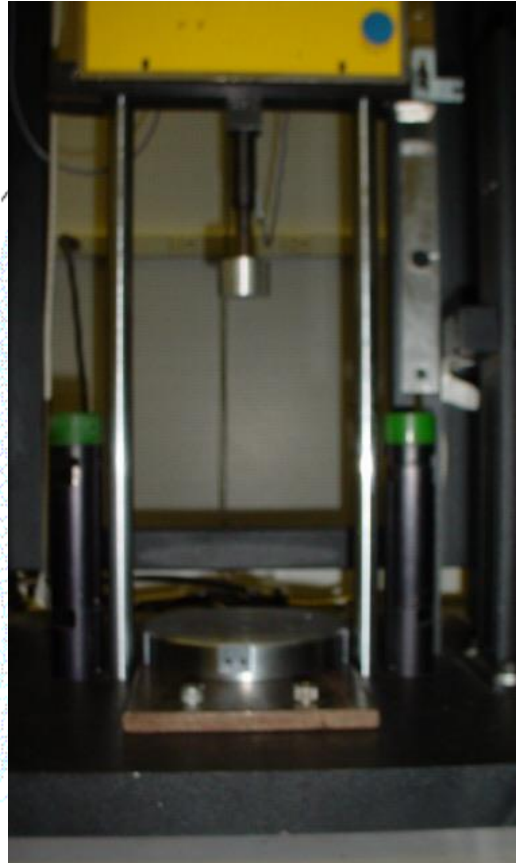
Test Strategy

- **Compressive stress-strain**
 - ▶ 5 decades of strain rate
 - .01, .1, 1, 10, 100 /s
 - ▶ Temperatures
 - -100 to 150C
- **Optional tests**
 - ▶ Tensile (for cut-off stress)
 - ▶ Shear (as required)

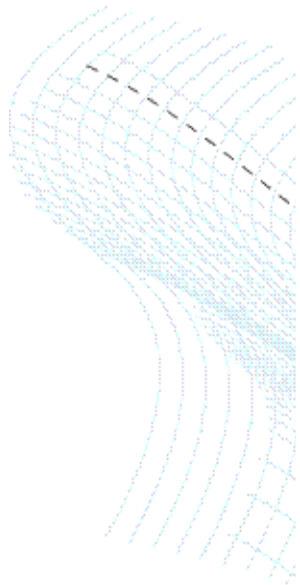
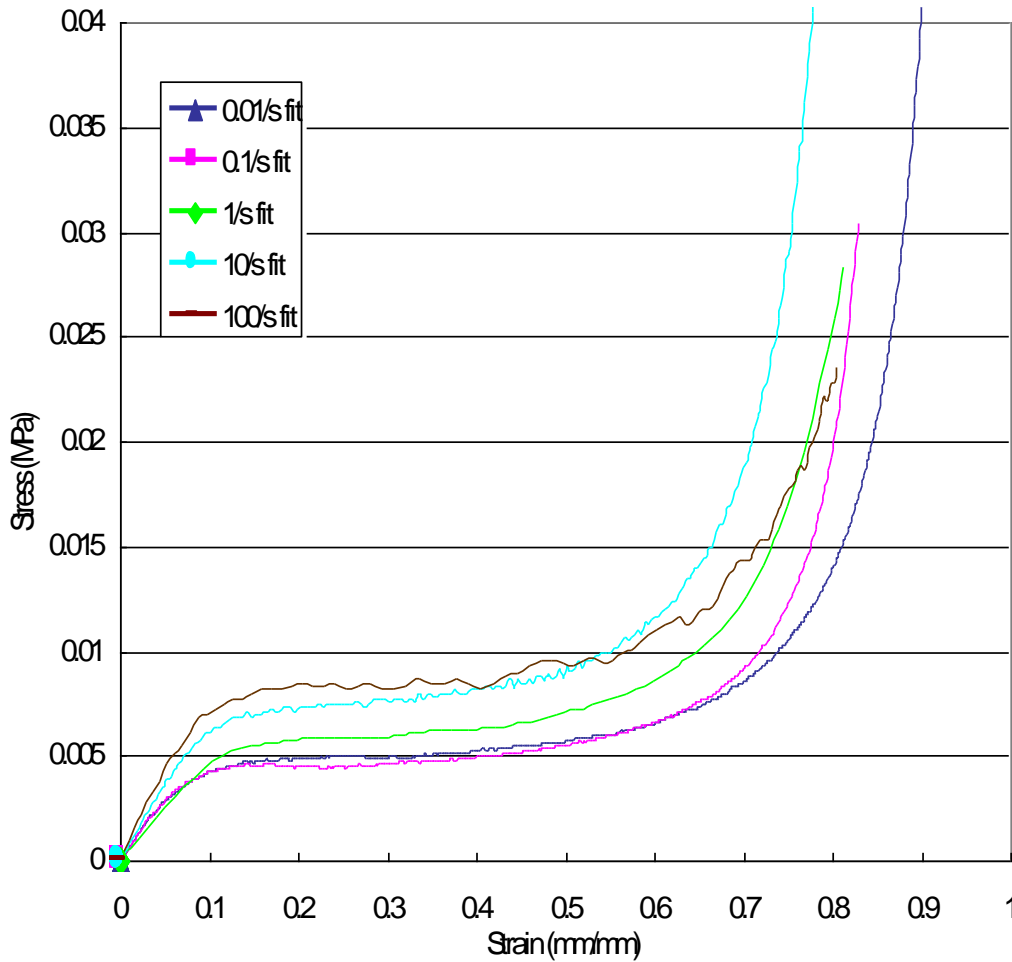


Hisp_comp.mpg

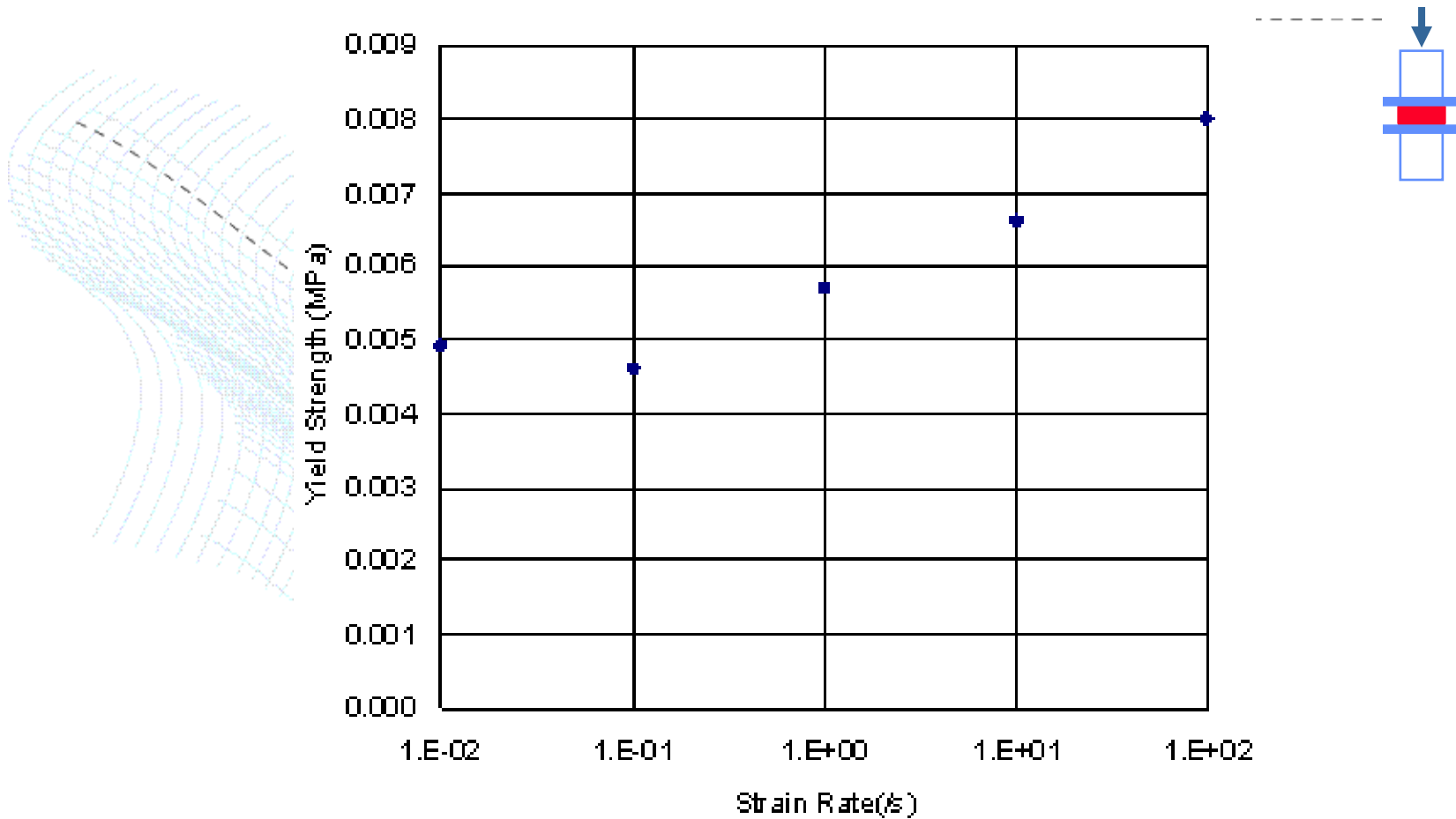
Test Instruments



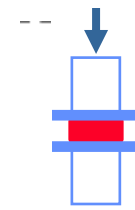
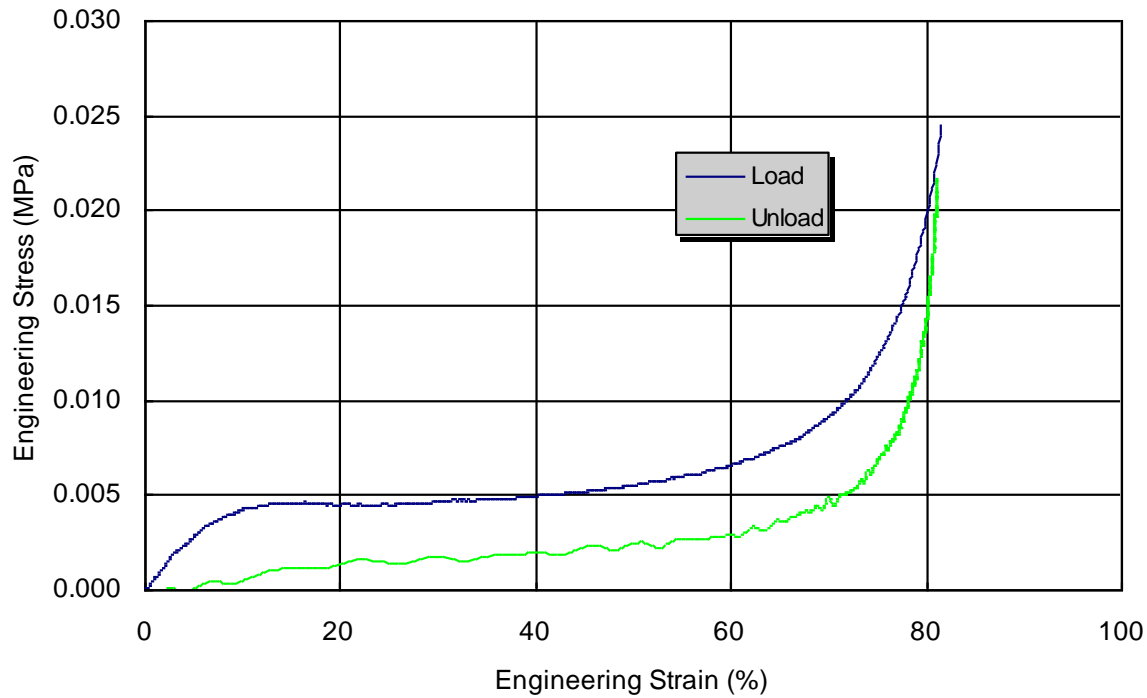
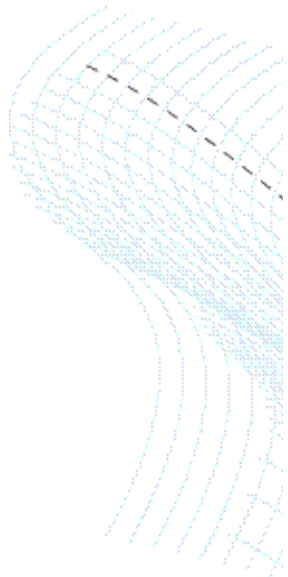
PU Foam-stress strain



PU Foam- rate effects



PU Foam recovery



Conclusions

- Choice of material model depends on
 - ▶ material
 - ▶ test data
 - ▶ situation complexity
- Proper selection = reasonable model
- Simple improvements can add power
- Validated models represent baseline
- Models can be tuned for multi-axial loadings

